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https://journals.sagepub.com/doi/10.1177/11795972241266705

DOI: 10.1177/11795972241266705

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Multidirectional Stimulation in an Isolated Murine Heart: A Computational Model

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Biomedical Engineering and Computational Biology Volume 15: 1–7 © The Author(s) 2024 Article reuse guidelines: sagepub.com/journals-permissions DOI: 10.1177/11795972241266705



ABSTRACT: It is common to use very high electric fields (E) to defibrillate hearts, which can damage cardiomyocytes, showing the importance of developing methods that can decrease the E applied in defibrillation protocols. We used COMSOL Multiphysics software to model, simulate, and analyze the application of an E in an isolated heart with monodirectional and multidirectional stimuli, using 2 pairs of electrodes and the superposition principle as a way to decrease the E applied and reduce the required number of stimulation electrodes. When applying an E of 3V/cm in the 0° , 30° , and 60° directions, individually in the stimulation chamber, E was equal to 3.2V/cm and its phases were equal to 0° , 30° , and 60° , respectively, validating the superposition principle. We observed a reduction up to 31.8% in |E| when applying a multidirectional stimulus when comparing to the monodirectional stimulus, in order to stimulate the same area of the heart. For the same amount of stimuli directions, we obtained up to 11.7% reduction of |E|, just by modifying the directions of the applied stimuli. In the simulation developed in this work, the superposition principle was validated in a stimulation chamber. For the same stimulated area, the multidirectional E has been always lower than the monodirectional. We observed that, in order to decrease the intensity of E, both the number of applied stimuli and their directions were relevant issues.

KEYWORDS: Computational modeling, defibrillation, electric field, multidirectional stimulus, superposition principle

RECEIVED: July 26, 2023. ACCEPTED: June 20, 2024.

TYPE: Original Research Article

FUNDING: The author(s) disclosed receipt of the following financial support for the research, authorship, and/or publication of this article: The authors would like to thank CAPES (Proc. N 88887.470307/2019-00) for the financial support.

DECLARATION OF CONFLICTING INTERESTS: The author(s) declared no potential conflicts of interest with respect to the research, authorship, and/or publication of this article.

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Introduction

Diseases affecting heart rhythm can present different etiologies, such as structural heart diseases, myocardial ischemia, and even events such as traumatic accidents. Among the cardiac arrhythmias, the ventricular ones represent a great risk to life, due to their direct relation in the ejection of blood into the pulmonary and systemic circulation. Ventricular Fibrillation (VF), characterized by the asynchronous activation of ventricular cells, is considered the most lifethreatening, and can lead to death, since only about 30% of patients survive them.¹

The only known therapy to reverse VF is defibrillation, which consists in the application of high intensity electric fields (E) directly into the heart or through the chest, in order to stimulate simultaneously between 75% and 90% of the ventricular myocytes.²

VF must be treated urgently, as the probability of the patient's death increases by 10% every minute without treatment. Few cases of defibrillation are successful after 10 minutes of its initiation.^{3,4}

However, a high intensity E applied to defibrillation can cause irreversible effects on the heart muscle, and may lead to temporary electrical and contractile dysfunction, cell death, and even trigger another $\rm VF.^5$

On the other hand, during stimulation, an E high enough to stimulate a large number of cardiac cells is required. The interaction of E with the heart is complex, due to its shape and the fact that the cardiac cells are oriented in different directions on

the heart. So in a defibrillation protocol, some cells will be exposed to E of magnitudes below $1\,\mathrm{V/cm}$, insufficient to stimulate them,⁶ and other cells will be exposed to E of magnitudes greater than $100\,\mathrm{V/cm}$, which can be lethal,⁷ such as those that are close contact with the defibrillator electrodes.⁸

In previous studies, it has been proven that the intensity of the stimulus applied to the cell major axis is half of that required to the cell minor axis, either for measuring the stimulation threshold or lethality.⁷

Thus, prioritizing stimulation in the major axis is a way to minimize the E applied to the heart, which decreases cell death. However, cardiac cells are positioned in different directions in the heart, thus, it would be necessary to vary the direction of the E by applying sequential stimuli in different directions (multidirectional stimulation).⁹

Fonseca et al⁹ used multidirectional stimulation (3 directions) in a population of randomly oriented isolated cardiac myocytes and observed that a larger number of cells were stimulated with multidirectional stimuli compared with a monodirectional stimulus of same magnitude.

Viana et al¹⁰ used a multidirectional defibrillator (3 directions) and observed a 30% decrease in the energy required to reverse VF in a population of pigs.

However, for multidirectional stimulation and defibrillation at least 3 pairs of electrodes are necessary (one for each direction), which in some preparations may be impractical, because placing 3 electrode pairs on the patient's body can be

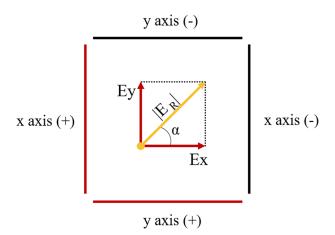


Figure 1. Schematic of 2 pairs of electrodes (red and black plates) generating E_R (in yellow) from 2 stimuli (E_x and E_v —in red).

a time-consuming task. Also, if we want to increase the number of stimulus directions, it would be needed to increase the number of electrode pairs. Therefore, in this paper we propose a method for multidirectional stimulation using only 2 pairs of electrodes, regardless of the number of stimulus directions, using the superposition principle.

Sabo et al¹¹ demonstrated that using one pair of electrodes (parallel plates) we can calculate the E inside a chamber by means of equation (1).

$$E = \pm \frac{I}{\sigma hl} \tag{1}$$

where E is the electric field for a single pair of stimulation electrode, I is the stimulation current, b is the height of Krebs-Henseleit solution, I is the electrodes width, and σ is the solution conductivity inside the chamber.

Assuming the use of 2 electrode pairs connected at different grounds and that its use does not affect the uniformity of E, we can use the same solution (equation (1)), 11 with the 2 electrode pairs orthogonally positioned to each other, using the superposition principle. The superposition principle demonstrates that the vector sum of the E generated by each axis is equal to the resulting $E(E_R)$ as we can see in Figure 1 and equations (2) and (3).

$$E_R = \sqrt{(E_x)^2 + (E_y)^2}$$
 (2)

$$\alpha = \arctan\left(\frac{E_y}{E_x}\right) \tag{3}$$

where E_R is the resultant electric field, E_x and E_y are the linear contribution of electric field intensity of each axis, and α is the angle that E_R is positioned in reference to the x axis.

Thus, by rapidly varying the amplitude of each independent stimulus source, it is possible to change the direction and amplitude of the stimulus, making it possible to stimulate the heart in multiple directions. The number of directions is limited by each pulse duration and the cell refractory period, since it is undesirable for the same cell to be stimulated more than once.

Therefore, the aim of this work is to develop a simulation in the software COMSOL Multiphysics® to analyze the effects of E in a stimulation chamber and in an isolated murine heart, when applying monodirectional and multidirectional stimuli.

Methods

In this work a computer simulation was developed in the software COMSOL that applied monodirectional and multidirectional stimuli in a stimulation chamber and in an isolated murine heart, with 2 pairs of electrodes, in order to validate the superposition principle and compare the effects of E in these cases.

Next, we will detail the stimuli applied, as well as their calculations; the construction of the stimulation chamber and the isolated heart; the mathematical model used in this simulation and the analyses that were performed.

Monodirectional and multidirectional stimuli

In order to apply monodirectional and multidirecional stimuli we need 2 parameters: the magnitude of E_R and the direction we want to stimulate the heart (α) . In order to apply E_R in an (α) direction, we first need to calculate the E generated by each axis:

$$Ex_n = E_R \cdot cos(\alpha) \tag{4}$$

$$Ey_n = E_R \cdot sin(\alpha) \tag{5}$$

Where n varies and corresponds to the number of the pulse applied in the x and y axes.

Isolating the current I in equation (1) and replacing E by or Ey_n , we calculate the value of the current applied in the stimulation chamber, for every pulse, by both axes. Then, with the value of the current for each pulse in a given direction, we calculate the value of the voltages applied by each axis by means of the equation (6).

$$V = \frac{I}{G} \tag{6}$$

Where *G* is the conductance of the stimulation chamber filled with Krebs-Henseileit's solution, calculated for this work.

For example, if we want to apply a monodirectional stimulus, where $E_R = 3 \text{ V/cm}$ and $\alpha = 0^\circ$, we would calculate as follows:

$$Ex_1 = 3 \cdot cos(0) \tag{7}$$

$$Ey_1 = 3 \cdot \sin(0) \tag{8}$$

The results of these calculations are $Ex_1 = 3 \text{ V/cm}$ and $Ey_1 = 0 \text{ V/cm}$.

Given these values, and knowing that $\sigma_{sol} = 0.015 \text{ S/cm}$, b = 4 cm, and l = 14 cm, we can calculate Ix_1 and Iy_1 by isolating the current in equation (1), so we have equations (9) and (10).

$$Ix_1 = 3 \cdot 0.015 \cdot 4 \cdot 14$$
 (9)

$$Iy_1 = 0 \cdot 0.015 \cdot 4 \cdot 14 \tag{10}$$

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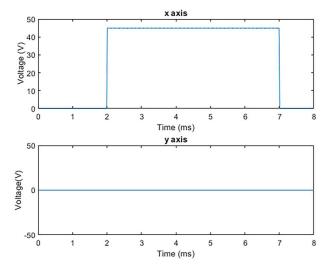


Figure 2. Example of a monodirectional stimulus applied with the superposition principle, when $E_R=3\,\mathrm{V}$ / cm and $\alpha=0^\circ$.

The results of these calculations are $Ix_1 = 2.52 \text{ A}$ and $Iy_1 = 0 \text{ A}$.

With these results we can calculate Vx_1 and Vy_1 in equations (11) and (12).

$$Vx_1 = \frac{2.52}{0.056} \tag{11}$$

$$Vy_1 = \frac{0}{0.056} \tag{12}$$

The results of these calculations are $Vx_1 = 45 \text{ V}$ and $Vy_1 = 0 \text{ V}$. In Figure 2 we can see the pulses related to that case. The same calculation is used for all pulses in the multidirectional stimuli. In Figure 3 we can see a multidirectional stimulus where $E_R = 3 \text{ V/cm}$ and $\alpha = 0^\circ$, 30° and 60° , applied sequentially.

For monodirectional stimulation, a voltage pulse with duration of 5 ms will be applied to the electrodes aligned with the α -axis. For multidirectional stimulation at least 3 pulses will be applied in each axis. Their duration is also 5 ms, and there is a 1 ms gap between pulses.

These pulses were created in a stimulation signal generation function in MATLAB R2021a software (Mathworks, USA). Once generated, the pulses were imported to COMSOL, where the simulation was carried out.

Geometry

The modeling geometry can be divided into 2 parts: stimulation chamber and isolated heart.

Stimulation chamber

The chamber (Figures 4 and 5) was inspired by the work of Antoneli et al.¹²

The chamber's dimensions are $15\,\mathrm{cm} \times 15\,\mathrm{cm}$. These dimensions were calculated so that the E_R would vary at

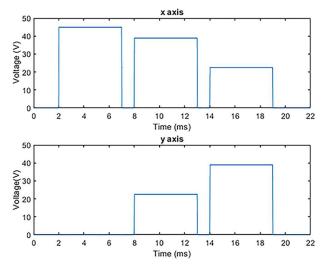


Figure 3. Example of a multidirectional stimulus applied with the superposition principle, when $E_R=3~V$ / cm and $\alpha=0^\circ,30^\circ$ and 60° .

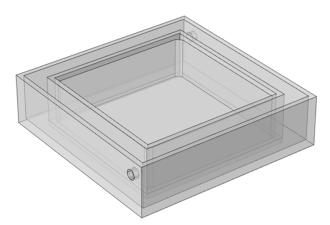


Figure 4. Stimulation chamber used in this simulation.

maximum 1% in modulus and 1° in phase in the central portion of the chamber.

The chamber is filled with Krebs-Henseleit solution at 37°C. On its inner sides are positioned the stimulation electrodes. The 4 plates that form the electrodes have equal dimensions, so that it is possible to apply the superposition principle. The electrodes are 14 cm width, and the submerged part of the stimulation electrodes is 4 cm height. The dimensions of the chamber and the submerged part of the stimulation electrodes were designed to obtain a homogeneous E.

Heart

The heart was represented by joining 2 geometries, a half-sphere and a half-ellipsoid. The sphere has radius R=1 cm, and the ellipsoid has dimensions a=2 cm and b=c=1 cm. The 2 geometries were cut in half and joined together, forming a simplified representation of a heart, as can be seen in Figure 6.

The heart surface area was calculated with $A = 17.02 \text{ cm}^2$.

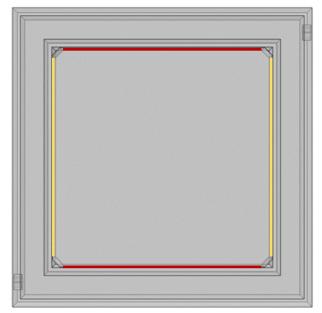


Figure 5. Top view of the chamber. The yellow electrodes represent one stimulation direction (*x* axis), while the red electrodes represent another stimulation direction (*y* axis).

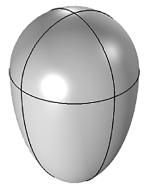


Figure 6. Representation of the heart used in the simulation.

The dimensions were based on a real murine heart aged 5 to 6 months old, which is the average age of the animals used in ex vivo biological experiments.

Mathematical model

The numerical simulation was performed to evaluate the distribution of E inside the stimulation chamber, so that the thermal analysis of the model was not considered. Therefore, to study the E, we used the Laplace equation, applied by the physics of Electric Currents in the COMSOL software. In this physics, the Laplace equation is applied by the formula:

$$-\nabla \left(\sigma \nabla V\right) - \varepsilon_0 \varepsilon_r \nabla \left(\frac{\partial}{\partial t} \left(\nabla V\right)\right) = 0 \tag{13}$$

where V is the electrical potential (V), σ is the electrical conductivity (S/m), ε_0 is the permittivity in vacuum (e), ε_r is the relative permittivity in the domain.

Two physics were used, one for each pair of electrodes, in order to isolate the 2 axes. The boundary conditions used were Ground and Terminal to define the potential to be applied by the electrodes, and 2 Current Conservation conditions, one for the chamber and one for the heart, for each axis. The mesh was automatically created by the generation COMSOL method for finer element sizes. The mesh has 15 205 elements, all of which are tetrahedra.

The parameters used in the simulation are presented in Table 1.

Analysis of the effect of E

Analysis of the E inside the chamber using the superposition principle. The chamber was filled with K-H solution $\left(\sigma_{sol}=1.5~{\rm S}\,/{\rm m}\right.,\,\varepsilon_{r_{sol}}=76\right).^{13}$ It was then applied an E_R of 3 V/cm with monodirectional stimuli in the directions $\alpha=0^\circ,\,\alpha=30^\circ,\,{\rm and}\,\,\alpha=60^\circ.$

Analysis of the E in the isolated heart

The heart $\left(\sigma_{\textit{heart}} = 0.16 \text{ S/m}\right)$, $\varepsilon_{r_{\textit{heart}}} = 94.10^6$ 14 was placed in the center of the chamber, which was filled with K-H solution. Then, we applied different magnitudes of E_R in the chamber, as follows:

- Monodirectional stimuli in the directions $\alpha = 0^{\circ}$, $\alpha = 30^{\circ}$, and $\alpha = 60^{\circ}$.
- Multidirectional stimuli (3 pulses) in the directions $\alpha = 0^{\circ}$, 30°, 60° and $\alpha = 0^{\circ}$, 45°, 90°.
- Multidirectional stimuli (4 pulses) in the directions $\alpha = 0^{\circ}$, 30° , 45° , 60° and $\alpha = 0^{\circ}$, 30° , 60° , 90° .

Results

Analysis of the E inside the chamber using the superposition principle

In Figure 7 we can see the E_R in the interior of the stimulation chamber in V/cm. The greatest variation of E is found near the electrodes, as expected, and in the center of the chamber the E_R is equal to 3.2 V/cm.

In Figure 8 we can see the direction with which E_R is being applied, which in this case is $\alpha = 0^{\circ}$.

For the 30° and 60° directions, the value of E_R inside the chamber was the same as that obtained in the 0° direction (3.2 V/cm), and the phase of E was 30° and 60°, respectively.

Analysis of the E in the isolated heart

In Figure 9 we can see the isolated heart being stimulated with a monodirectional $E_R = 3 \text{ V/cm}$ in the 0° (Figure 9A), 30° (Figure 9B), and 60° (Figure 9C) directions. The area in red represents the part of the heart that is stimulated with at least

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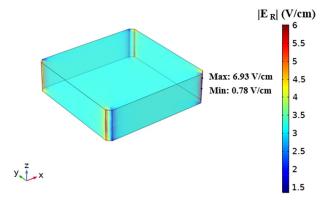


Figure 7. Electric field inside the chamber in V/cm when the E_R applied is equal to 3 V/cm and $\alpha = 0^{\circ}$.

Table 1. Simulation parameters.

PARAMETER (UNIT)	SYMBOL	VALUE
Temperature (K)	Т	310.15
Solution electrical conductivity (S/m)	σ _{sol}	1.5
Solution relative permittivity	ε _r sol	76
Heart electrical conductivity (S/m)	σ _{heart}	0.16
Heart relative permittivity	ε _r heart	94×10 ⁶

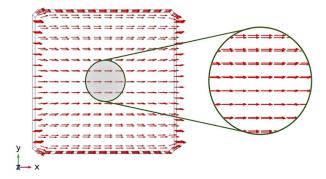


Figure 8. Phase of the electric field inside the chamber in V/cm when $E_R=3~{\rm V}$ / cm and $\alpha=0^{\circ}$.

 $4.5 \,\mathrm{V/cm}$, which represents $7.68 \,\mathrm{cm^2}$, or 45.12% of the surface area, in each direction, as shown in the animations (Online Resource 1, 2, and 3).

Knowing that in order to defibrillate a heart it is necessary to simultaneously recruit between 75% and 90% of the ventricular myocytes,² in the case of monodirectional stimulation we would need an E_R of 3.8 and 4.4 V/cm, respectively.

In Figure 10 we can see the isolated heart being stimulated with an $E_R = 3 \text{ V/cm}$ when $\alpha = 0^\circ$, 30°, and 60°, applied sequentially, with 1 ms gap between directions. The area in red represents the part of the heart that is stimulated with at least 4.5 V/cm, which represents 12.87 cm², or 75.6% of the total

surface area of the heart, which would be sufficient for defibrillation to take place, as shown in the animation (Online Resource 4). To recruit 90% of the surface area, we would need an E_R equal to 3.4 V/cm, as shown in the animation (Online Resource 5).

In Figure 11 we can see the comparison of the monodirectional stimulus $(\alpha=0^\circ)$ and the multidirectional stimulus when we applied 3 pulses $(\alpha=0^\circ,30^\circ \text{and } 60^\circ)$. It can be observed that for the same stimulated area, the modulus of the multidirectional E is always lower than the monodirectional.

The result from varying the direction of the stimulus and increasing the number of directions in which E is applied can be observed in Figures 12 and 13, respectively. By varying the directions of the multidirectional stimuli, we can observe that the magnitude of E is lower for the same stimulated area of the heart, when applying 3 stimuli in $\alpha = 0^{\circ}, 45^{\circ}, 90^{\circ}$ when compared to the E applied in $\alpha = 0^{\circ}, 30^{\circ}, 60^{\circ}$.

By increasing the directions of the stimuli to 4, we can observe the same effect: for the same stimulated area of the heart, when applying 4 stimuli in $\alpha = 0^{\circ}, 30^{\circ}, 60^{\circ}, 90^{\circ}$ the E is lower when compared to the stimulus applied in $\alpha = 0^{\circ}, 30^{\circ}, 45^{\circ}, 60^{\circ}$.

Discussion

In the literature we can find several studies on multidirectional stimulation, ^{9,10} but no one with only 2 electrode pairs.

In the simulation developed in this work, the superposition principle was validated in a stimulation chamber. The small difference found in the value of E_R can be explained by the arrangement of the electrodes in the chamber—they are positioned in such a way that they do not touch each other, so that it is possible to apply the superposition principle—and this is not taken into account in the calculation.

Regardless, the results are very close to what was calculated, showing the effectiveness of the superposition principle when applying an E to a stimulation chamber using 2 pairs of electrodes.

When we compare the monodirectional and the multidirecional stimuli applied to the heart, we can observe that for the same stimulated area, the modulus of the multidirectional E is always smaller than the monodirectional, as it was expected. We observed a decrease up to 31.8% in $\mid E \mid$ in this case.

From the results found we can observe that, to decrease the intensity of E, not only does the number of stimuli applied matter, but also the directions in which we are applying them. It is possible to realize this because by applying an E_R in $\alpha = 0^\circ, 45^\circ, 90^\circ$, we stimulate the same percentage of area as applying the E_R in $\alpha = 0^\circ, 30^\circ, 60^\circ, 90^\circ$. We also observed this effect, because by changing stimulus directions, without increasing the amount of stimuli, it was also possible to decrease |E| by up to 11.7%.

Therefore, with 2 pairs of electrodes we can apply as many stimuli as necessary, in different directions and with different

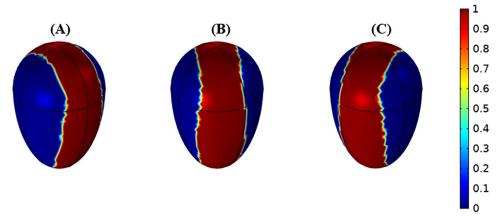


Figure 9. Representation of an isolated heart being stimulated with a monodirectional E_R equal to 3V/cm in the 0° (A), 30° (B), and 60° (C) directions. The area in red is stimulated with at least 4.5 V/cm.

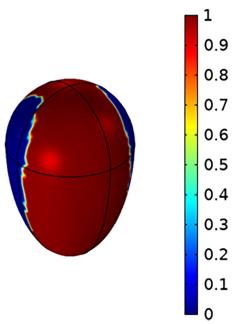


Figure 10. Representation of an isolated heart being stimulated with a multidirectional E_R of 3 V/cm in the 0°, 30°, and 60° directions, sequentially. The area in red is stimulated with at least 4.5 V/cm.

amplitudes, as a way to decrease the applied $\mid E_R \mid$, as long as the total duration of the pulses does not exceed the absolute refractory period of the cardiac myocytes.

In order to understand in greater depth—as well as validate—the effect of applying monodirectional and multidirectional stimuli using the superposition principle, it would be interesting to develop ex vivo experiments with murine hearts, applying the techniques reported in this study.

Furthermore, computational modeling is emerging to be a very important step in the advancement of cardiovascular research by enhancing innovations in cardiac study.

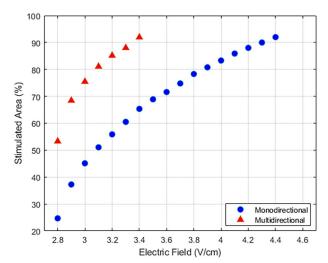


Figure 11. Comparison between monodirectional ($\alpha = 0^{\circ}$, circles) and multidirectional ($\alpha = 0^{\circ}$, 30°, 60°, triangles) stimuli.

Conclusion

This simulation study aimed to use the COMSOL Multiphysics software to model, simulate, and analyze the application of an E in an isolated heart with monodirectional and multidirectional stimuli, using 2 pairs of electrodes and the superposition principle as a way to decrease the E applied and reduce the required number of stimulation electrodes.

The superposition principle was validated in the stimulation chamber, and we observed that, in order to decrease the intensity of E we should use multidirectional stimulation, and that both the number of applied stimuli and their directions were relevant issues.

Finally, the verified results allow future biological experiments with isolated hearts in which the same results obtained from this simulation shall be investigated. If the results are positive, this may enable the development of an effective defibrillator device built under these principles, what may be an important advance in cardiology and arrhythmia treatment.

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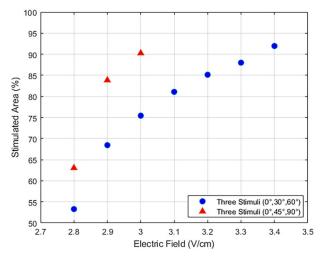


Figure 12. Comparison between multidirectional stimuli applied in 3 directions, when $\alpha = 0^{\circ}, 30^{\circ}, 60^{\circ}$ (circles) and $\alpha = 0^{\circ}, 45^{\circ}, 90^{\circ}$ (triangles).

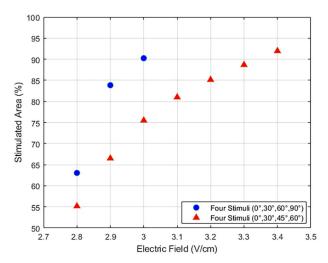


Figure 13. Comparison between multidirectional stimuli applied in 4 directions, when $\alpha=0^{\circ},30^{\circ},60^{\circ},90^{\circ}$, (circles) and $\alpha=0^{\circ},30^{\circ},45^{\circ},90^{\circ}$ (triangles).

Author Contributions

Lizandra Sá: Conceptualization, Methodology, Formal analysis, Investigation, Writing - Original Draft, Visualization.

Jorge Costa Jr: Methodology, Writing - Review & Editing.

Lindemberg Silveira-Filho: Writing - Review & Editing, Supervision. Pedro de Oliveira: Conceptualization, Methodology, Writing - Review & Editing, Supervision.

Supplemental Material

Supplemental material for this article is available online.

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